



Jun *30, 2022* 

Dear Water Warriors,

TDS transfer from water (Feed) into water (Reject) is an interesting water treatment technology, where we concentrate the impurities in small quantity of water making rest of the water free of TDS.

Reverse Osmosis is in in every process scheme these days and we use software to design and optimize the right RO system.



This issue of 'Waughter', we requested SSr to design a plant for us and explain the way he thinks.

Let's design together.

Nidhi Jain – Civil Engineer

#### Down the Memory Lane.. IMS Design

Was the First software Sanjeev Srivastava our Lead Technology ever used. Over the years many other software and Knowledge Partners also contributed to improving design thinking: Dupont, Dow, Suez, Toray, CSM, these names became synonym to Reverse Osmosis Know how and all are good.





He still remembers his first design, that was done through complicated Integral Calculus method manually without software. Unfortunately, he does not have hand notes of that and has forgotten manual calculations now.

#### Defining the Input Required for RO Design?

In order to design a good RO system, one must have all the data mentioned in below table:

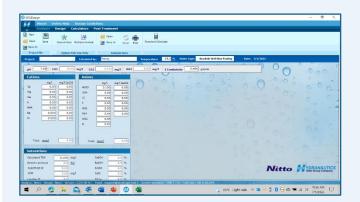
Sr No	Description	Unit	Value
1.01	Treated Water Quantity	m³/d	600
1.02	RO Operating hours	h	24
1.03	Permeate Flow Rate	m³/h	25
1.04	Feed Water Source		Borewell
	Feed Water Quality		
2.01	TDS	mg/l	2310
2.02	Conductivity	μS/Cm	3513
2.03	рН	-	7.8
2.04	TSS	mg/l	12
2.05	Turbidity	mg/l	6
2.06	Hardness	mg/l as CaCO3	250
2.07	Ca Hardness	mg/l as CaCO3	150
2.08	Mg Hardness	mg/l as CaCO3	100
2.09	Na+K	mg/l	By Calculation
2.10	Chloride	mg/l as Cl	700
2.11	Sulphate	mg/l as SO4	135
2.12	Nitrate	mg/l as NO3	12
2.13	M-Alkalinity	mg/l as CaCO3	210
2.14	P-Alkalinity	mg/l as CaCO3	0
2.15	Phosphate	mg/l as PO4	1
2.16	Boron	mg/l as B	0.1
2.17	Reactive Silica	mg/l as SiO2	23
2.18	F,NH4,Ba,Sr etc	mg/l as Such	If Available
	Treated Water Quality		
3.01	TDS	mg/l	100
3.02	Hardness	mg/l as CaCO3	10
3.03	Reactive Silica	mg/l as SiO2	1

#### Before you design.. with us together!

For the given data if you wish to design together for better learning. Please:

- 1. Read Waughter Volume 1 Edition 7
- 2. Download IMS Design on your computer

Once down you will reach the WINDOW as shown below



Now follow magazine and software together.



# Pure CODe

## **COD** REDUCTION MEDIA

PureCODe is an absorbent media for the **lowering of recalcitrant COD** (Fine polishing of tough to treat COD) which subsequently helps in meeting stringent discharge norms in various industries such as textiles, chemicals, pharmaceuticals, etc. **This media is also regenerable on-site.** 



PureCODe specialty media - helps in lowering COD significantly to meet stringent discharge norms and recycle maximum amout of water.

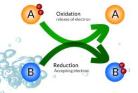
## **WORKING PRINCIPLES OF THE MEDIA:**



ABSORPTION (INSIDE THE MEDIA)



ADSORPTION
(SURFACE OF MEDIA)



REDOX
(OXIDATION REDUCTION)





+91 9820173817





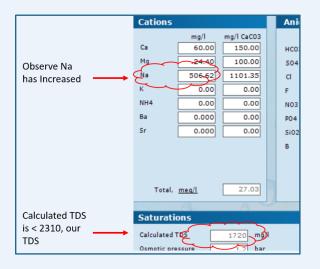


Jun *30, 2022* 

#### Feed Data into Software

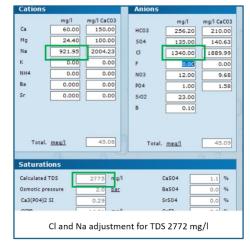
When we enter the data available to us, the software suggested see below: (Warning! 81% Difference in Ions). This is because Na + K is not yet entered.

We need to Click on Na to adjust the same.



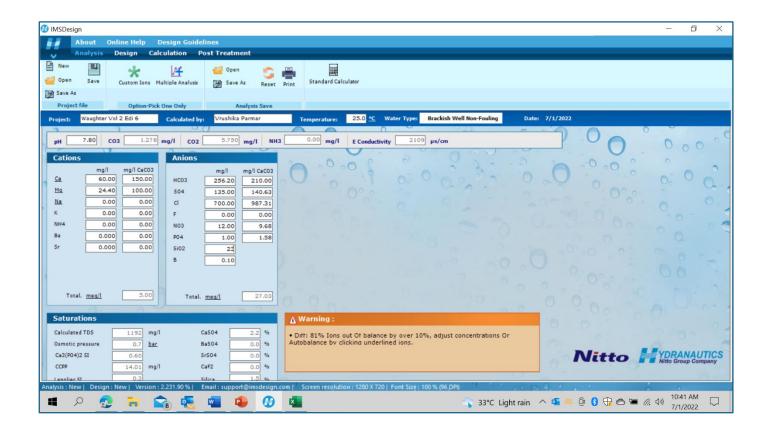
For TDS balance designer need to increase the Cl Value as well as Na value to reach design TDS of 2310 mg/l.

It is better to have 20% extra margin wrt to TDS. Remember Osmotic Pressure is directly proportional to the Feed TDS and thus 20% over design over design value is a good practice in designing RO system.



Press Save As above Analysis Save and Continue...

Temperature is an important no in design (25 deg C), at higher temperature Feed Pressure reduced and quality deteriorates and vice versa.









#### Design the RO system?

For a proper design we have several steps that need attention, let's move 1 by 1 to all steps and understand the significance of each.

#### Step 1

Understand Feed Water. For TDS up-to 8000 mg/l safely take Brackish Water RO membranes and above 22000 mg/I Sea Water RO membranes.

Selection of membrane also depends upon treated water quality. For stringent quality, you may have to select High Rejection membrane. (Feed Already Entered in previous Page)

#### Step 2

Define Recovery. One would like to go for highest recovery. High Recovery means less volume on Reject or more concentrated Reject. That means:

- a. Higher Osmotic Pressure barrier and hence high Feed
- b. Solubility Concerns of Ca\*HCO<sub>3</sub> and SiO<sub>2</sub>
- c. Long Train of RO elements, remember 1<sup>st</sup> element recovers max 15% and next 15% from the balance 85% and so on...

The point c above defines no of stages. Since we have 6 Element long Pressure Tube, beyond 6 Serial no of stages increase. Let's design for 75% Recovery, i.e. 2 stages.

System Recovery	No of Elements in Series	No of Stages
40-60	6	1
60-80	12	2
80-94	18	3

#### Step 3

Element Diameter. Membranes are available in dia 2.5", 4" & 8". Generally, for flow rate < 200 lph we use 2.5" element and flow > 3 m<sup>3</sup>/h we use 8" element. In between it's better to use 4" element.

For special reasons or if low recovery is acceptable e.g. RO plants on boats, designer may use 8" membrane even at lower flow rates.

#### Step 4

Flux Selection. Flux means productivity of membrane per m<sup>2</sup> of its surface used for Filtration of clean water. Naturally it depends upon the amount (concentration) of unwanted materials. SDI usually is the measure of presence of impurities before the water is Fed to Reverse osmosis element. A sample of Flux guidelines is attached (All Membrane Suppliers issue such guidelines in their software):

21-25 36-43 30 000 (34) 7, 000 (38) 8, 600 (40) 8, 600 (40) 8, 000 (42) 9, 10 (2.3) 10 (2.3)	SDI < 3 16-20 27-34 19 7,500 (28) 8,300 (31) 8,600 (33) 8,900 (34) 9,100 (34) 10,000 (38)	6,500 (25) 7,200 (27) 7,500 (28) 7,700 (29) 7,900 (30) 8,700 (33)	SDI < 5 12-16 20-27 15 num permeat 5,900 (22) 6,500 (25) 6,800 (26) 7,000 (26) 7,200 (27) 7,900 (30) m concentrat 15 (3.4)	5,300 (20) 5,900 (22) 5,900 (22) 6,300 (24) 6,400 (24) 7,100 (27)	4,700 (18) 5,200 (20) 5,200 (20) 5,500 (21) 5,700 (22) 6,300 (24)	Well or MF <sup>1</sup> SDI < 3 8-12 13-20 15 6,700 (25) 7,900 (30)	SDI < 5 7-10 11-17 13 6,100 (23)
21-25 36-43 30 000 (34) 7, 000 (38) 8, 600 (40) 8, 600 (40) 8, 000 (42) 9, 10 (2.3) 10 (2.3)	16-20 27-34 19 7,500 (28) 8,300 (31) 8,600 (33) 8,900 (34) 9,100 (34) 10,000 (38)	13-17 22-29 17 Maxin 6,500 (25) 7,200 (27) 7,500 (28) 7,700 (29) 7,900 (30) 8,700 (33) Minimu 13 (3.0)	12-16 20-27 15 num permeat 5,900 (22) 6,500 (25) 6,800 (26) 7,000 (26) 7,200 (27) 7,900 (30) m concentrat 15 (3.4)	10-14 17-24 14 e flow rate, gj 5,300 (20) 5,900 (22) 5,900 (22) 6,300 (24) 6,400 (24) 7,100 (27) te flow rate <sup>2</sup> ,	8-12 14-20 12 pd (m³/d) 4,700 (18) 5,200 (20) 5,500 (21) 5,700 (22) 6,300 (24) gpm (m³/h)	8-12 13-20 15 6,700 (25)	7-10 11-17 13
36-43 30 000 (34) 7,000 (38) 8,600 (40) 8,600 (40) 8,000 (42) 9,000 (45) 11 10 (2.3) 10 (2.3)	27-34 19 7,500 (28) 8,300 (31) 8,600 (33) 8,900 (34) 9,100 (34) 10,000 (38)	22-29 17 Maxim 6,500 (25) 7,200 (27) 7,500 (28) 7,700 (29) 7,900 (30) 8,700 (33) Minimu 13 (3.0)	20-27 15 num permeate 5,900 (22) 6,500 (25) 6,800 (26) 7,000 (26) 7,200 (27) 7,900 (30) m concentral 15 (3.4)	17-24 14 e flow rate, g 5,300 (20) 5,900 (22) 5,900 (22) 6,300 (24) 6,400 (24) 7,100 (27) te flow rate <sup>2</sup> ,	14-20 12 pd (m³/d) 4,700 (18) 5,200 (20) 5,200 (20) 5,500 (21) 5,700 (22) 6,300 (24) gpm (m³/h)	13-20 15 6,700 (25)	11-17 13 6,100 (23)
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10 (2.3) 10 (2.3)	13 (3.0)			16 (3.6)	18 (4.1)		
10 (2.3)		13 /3 (1)					
			15 (3.4)	18 (4.1)	20 (4.6)		
	13 (3.0)	13 (3.0)	15 (3.4)	18 (4.1)	18 (4.1)		
25 (5.7)	25 (5.7)	25 (5.7)	25 (5.7)	25 (5.7)	25 (5.7)		
10 (2.3)	13 (3.0)	13 (3.0)	15 (3.4)	16 (3.6)	18 (4.1)	13 (3.0)	15 (3.4)
a Maximum feed flow rate <sup>2</sup> , gpm (m³/h)							
65 (15)	65 (15)	63 (14)	58 (13)	52 (12)	52 (12)		
75 (17)	75 (17)	73 (17)	67 (15)	61 (14)	61 (14)		
75 (17)	75 (17)	73 (17)	67 (15)	61 (14)	61 (14)		
85 (19)	75 (17)	73 (17)	67 (15)	61 (14)	61 (14)		
65 (15)	65 (15)	63 (14)	58 (13)	52 (12)	52 (12)	63 (14)	56 (13)
72 (16)	72 (16)	70 (16)	64 (15)	58 (13)	58 (13)	70 (16)	62 (14)
7 7 8	5 (17) 5 (17) 5 (19) 5 (19) 5 (15) 2 (16) cess using a p across a sin igning at max	5 (17) 75 (17) 5 (17) 75 (17) 5 (19) 75 (17) 5 (19) 75 (17) 5 (15) 65 (15) 2 (16) 72 (16) coses using a membrane will place across a single element is signing at maximum of 80%	5 (17) 75 (17) 73 (17) 5 (17) 75 (17) 73 (17) 5 (19) 75 (17) 73 (17) 5 (15) 65 (15) 63 (14) 2 (16) 72 (16) 70 (16) coses using a membrane with pore size of- o acrose a single element in 15 paid (1bar) signing at maximum of 80% (12 paid) for any	$\begin{array}{lll} 5(17) & 75(17) & 73(17) & 67(15) \\ 5(17) & 75(17) & 73(17) & 67(15) \\ 5(19) & 75(17) & 73(17) & 67(15) \\ 5(16) & 57(17) & 73(17) & 67(15) \\ 5(16) & 55(15) & 63(14) & 68(13) \\ 2(16) & 72(16) & 70(16) & 64(15) \\ \cos \omega \sin a \ amerborne \ with pole \ uice of \ d 5 \ micm \ a \ one of \ uice of \ d 15 \ micm \ a \ one of \ uice of $	\$ (17)	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

In our case let's take Borewell water treated with conventional sand filter and select the flux as 28 l/m<sup>2</sup>.h (range 27 -34 l/m<sup>2</sup>.h)

#### Step 5

Membrane Area Calculation. Since we have flow rate as 25 m<sup>3</sup>/h and we have selected flux as 28 l/m<sup>2</sup>.h, her membrane Area required for our design is:

Membrane Area = Flow 
$$\div$$
 Flux  
= 25000 lph  $\div$  28 l/m<sup>2</sup>.h  
= 892 m<sup>2</sup> = 9607 ft<sup>2</sup>

So, our design shall have X Nos of membrane with Y ft<sup>2</sup> surface each membrane

and  $X.Y = 9607 \text{ ft}^2$ 





#### Step 6

Membrane Selection. In step 3 we understand 8" dia membrane is good for our design since flow rate is 25 m3/h.

Element type					
BW elements (365 ft <sup>2</sup>	) 1	10			
BW elements (400 ft <sup>2</sup>	and 440 ft <sup>2</sup> ) 1	10			
NF elements	1	10			
Full-fit elements	2	25			
SW elements	1	10			
	Active area				
Element type	ft² (m²)				
BW elements	365 (33.9)	65			
BW or NF elements	400 (37.2)	75			
BW elements	440 (40.9)	75			
Full-fit elements	390 (36.2)	85			
SW elements	320 (29.7)	65			
SW elements	380 (35.3)	72			
<sup>1</sup> MF: Microfiltration - co	<sup>1</sup> MF: Microfiltration - continuous filtration pro				
<sup>2</sup> The maximum recomn value is more limiting.		-			
Note: The limiting value guidelines results	s listed above have in a warning on the				

Close look of chart in Step 4 above suggests we have different elements with different active surface area. So let consider the membrane with Active Area of  $\sim 365 \text{ ft}2$ 

So our Nos of membranes required shall be

$$= 9607 \div 365 = 26.32$$
  
~ say 27

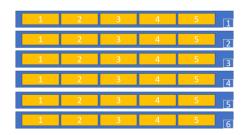
#### Step 7

<u>RO Pressure Tubes</u>. The 27 Nos membrane calculated above need to be put into pressure tubes. The standard length of the tubes are 1,2,3,4,5 & 6.

Further in Step 2 we understand the Nos of stage shall be 2. i.e. Reject of Stage 1 shall be Fed to Stage 2.

If we select 6 Element Pressure Tube, we will need 6\*5 = 30 membranes to fill all pressure tubes. If we select 5 Element Tube then we will need 5\*6 = 30 membranes to fill all pressure Tubes.

In short Total no of membranes used ÷ No of Elements in Tube shall be a whole number. Let's select the Pressure Tube length as 5 El Long, means 6 Pressure Tube. Like below:

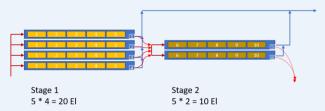


6 \* 5 = 30 membranes filled in 6 Pressure Tubes that are each 5 El long.

#### Step 8

Staging Ratio. No of stages we selected depends upon recovery and for 75% we selected 2. The last stage shall always have ½ the element of previous stage. So for a two stage system:

No of membranes in last stage  $(2^{nd})$  = A No of membranes in previous stage  $(1^{st})$  = 2A

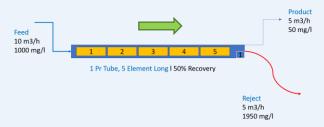


Thus 3A = 30 and A = 10. So our Staging would be as shown above. Here one can say that  $\sim 50\%$  recovery is achieved in stage 1 and 50% of 50% balance that is  $\sim 25\%$  is recovered is stage 2 making overall recovery as  $\sim 75\%$ .

Final 25% is reject water that is removing TDS that has been rejected by membrane.

#### Step 9

For 9<sup>th</sup> step, we need to understand the word "Integral Calculations", Look at below Pressure Tube and understand what's happening when water is flowing:



- a. Feed Flow is decreasing and becomes 5 m<sup>3</sup>/h at end as some of it becomes permeate.
- b. Osmotic Pressure keeps increasing as TDS becomes 1950 from starting 1000 mg/l
- c. Since Feed Pressure say ~ 12 kg/Cm², will keep reducing, NDP (Nett Drive Pressure = Feed Pr Osmotic Pr) will decrease.
- d. Thus, the Permeate production shall decrease as we travel down the tube means 1<sup>st</sup> element will produce most of the permeate and last the least.
- e. Bottom line: Flux is always reducing.





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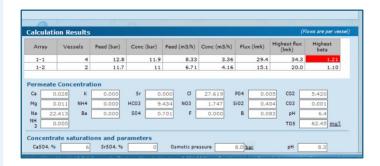
#### Step 10

<u>Software Use</u>. The design obtained from above 9 steps is transported on a software to perform calculations and check if the guidelines for membrane use are violated. One must balance the flow (Flux) to ensure:

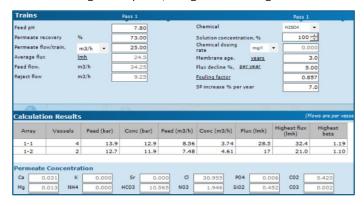
- a. Lead Element flux is not higher than the limit set.
- b. Brine leaving from last element should not be lower than defined value, else scaling/fouling. Minimum Sweep velocity to be maintained.
- c. Make better use (Flux) of tail end elements
- d. Many more reasons as we learn along

Our design as entered in software shall look as in below figures.

- A. Press Run to check if design is OK, the calculations are performed and we have:
  - 1. Beta High 1.21 marked in Red TDS < 63 mg/l as per our design.

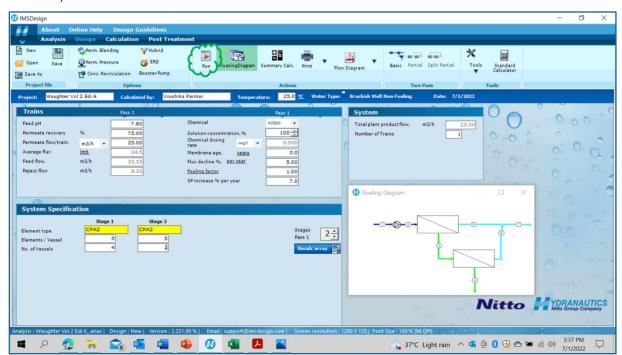


To correct Beta, reduce recovery and enter correct membrane age as 3 years, we get final design as:



The Screen shot of data entry, please mark membrane age 0 is a wrong entry it must be 3.

- Concentrate Recirculation is a way to increase recovery and control Beta Factor (Higher flow from lead element)
- Booster Pump design is to ensure better flux distribution through-out membrane train and energy optimization
- Permeate Back Pressure design controls higher flow from lead elements. Can pose engineering challenge while construction, be careful.



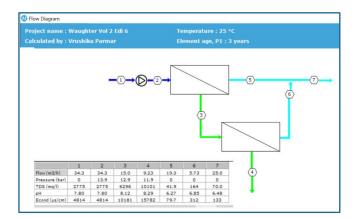




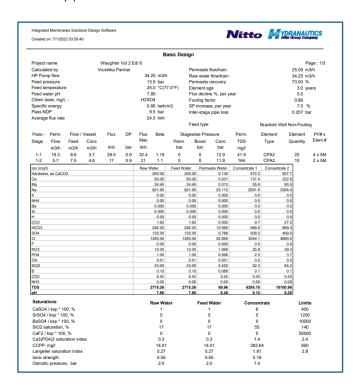
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#### Final Design

The Final design thus has 73% recovery, TDS < 70 mg/l and designer can take a complete 3 page print to see the design and performance of each element.



The PDF of 1st page of design is of interest wrt to solubility points:



The LSI of 1.8 indicates we need to add antiscalant.

Further SiO<sub>2</sub> saturation is in in limit so no worries, or else use antiscalant till SiO<sub>2</sub> in Concentrate 2 is up to 300 mg/l

For more practice and perfect your design.

### जल जीवन जननी!!



#### Our world is Waughter

The technical knowledge share attempt of Aktion Consultancy and the contents in the magazine shall be qualified by Sanjeev Srivastava our Technology Lead.

Our next edition focuses on: "UF Design & BOQ Generation"

Please feel free to write or contact Mrs. Neha Deshpande 95129 55227

Aktion Consultancy C 1305, Rajyash Rise New Vasana, Nr Vishala Circle, NH-08, Ahmedabad - 380 051 India



Alka Srivastava – Founder